FFT Advanced Tools for RSE and EMI Measurements under the view of CISPR-16-2-x

EUT Timing analysis for correct measurement time settings in receivers, spectrum analyzers or FFT-based instruments

Christian Reimer



Re-organization of CISPR16 Publications in 2003

				•
CISPR 16-1	Radio disturbance and immunity measuring apparatus		CISPR 16-1-1	Measuring apparatus
			CISPR 16-1-2	Ancillary equipment – Conducted disturbances
			CISPR 16-1-3	Ancillary equipment – Disturbance power
			CISPR 16-1-4	Ancillary equipment – Radiated disturbances
			CISPR 16-1-5	Antenna calibration test sites for 30 MHz to 1 000 MHz
CISPR 16-2	Methods of measurement of disturbances and immunity		CISPR 16-2-1	Conducted disturbance measurements
			CISPR 16-2-2	Measurement of disturbance power
			CISPR 16-2-3	Radiated disturbance measurements
			CISPR 16-2-4	Immunity measurements
		◀	CISPR 16-3	CISPR technical reports
CISPR 16-3	Reports and recommendations of CISPR		CISPR 16-4-1	Uncertainties in standardised EMC tests
			CISPR 16-4-2	Measurement instrumentation uncertainty
			CISPR 16-4-3	Statistical considerations in the determination of EMC compliance of mass- produced products
CISPR 16-4	4 Uncertainty in EMC measurements		CISPR 16-4-4	Statistics of complaints and a model for the calculation of limits



CISPR16-2 -1 / -2 / -3



CISPR 16-2-3

Edition 3.2 2014-03

INTERNATIONAL STANDARD

Specification for radio disturbance and immunity measuring apparatus and methods –

Part 2-3: Methods of measurement of disturbances and immunity – Radiated disturbance measurements

CISPR 16-2-1	Conducted disturbance measurements
CISPR 16-2-2	Measurement of disturbance power
CISPR 16-2-3 Edition 3.2 2014-03	Radiated disturbance measurements



CISPR16-2 -1 / -2 / -3 Minimum Scan Times

Table 1 – Minimum scan times for the three CISPR bands with peak and quasi-peak detectors

I	Frequency band	Scan time <i>T</i> s for peak detection	Scan time <i>T</i> s for quasi-peak detection
Α	9 kHz to 150 kHz	14,1 s	2 820 s = 47 min
В	0,15 MHz to 30 MHz	2,985 s	5 970 s = 99,5 min = 1 h 39 min
C and D	30 MHz to 1 000 MHz	0,97 s	19 400 s = 323,3 min = 5 h 23 min

Depending on the type of disturbance, the scan time may have to be increased – even for quasi-peak measurements. In extreme cases, the measurement time $T_{\rm m}$ at a certain frequency may have to be increased to 15 s, if the level of the observed emission is not steady (see 6.5.1). However isolated clicks are excluded.

X

Many sections of the 3 standard parts have the same content. Numbering and indices are different.

Scan time translates into...

- \rightarrow "dwell time" in a stepped scan (e.g. in receiver mode)
- \rightarrow "sweep time" in a swept scan (e.g. in analyzer mode)



CISPR16-2 all parts - since edition 1

6.5.2 Scan rates for scanning receivers and spectrum analyzers

One of two conditions need to be met to ensure that signals are not missed during automatic scans over frequency spans:

- for a single sweep: the measurement time at each frequency must be larger than the intervals between pulses for intermittent signals;
- for multiple sweeps with maximum hold: the observation time at each frequency should be sufficient for intercepting intermittent signals.

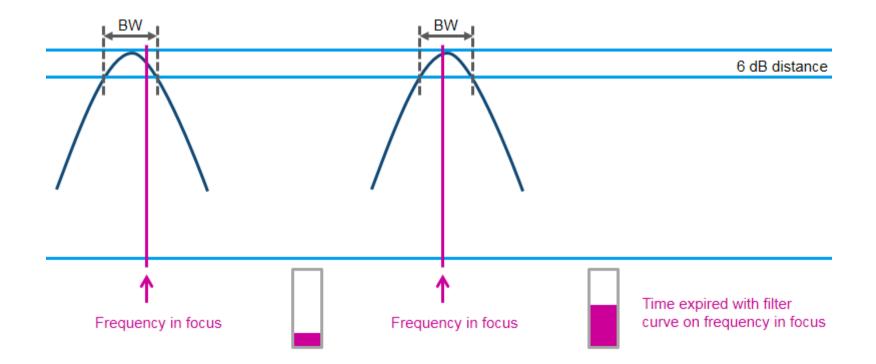
In focus of clause 6.5.2:

- the measurement time at each frequency
- intervals between pulses
- intercepting intermittent signals

The number of frequency points is an important parameter and needs to be considered especially in sweeps / analyzer mode.



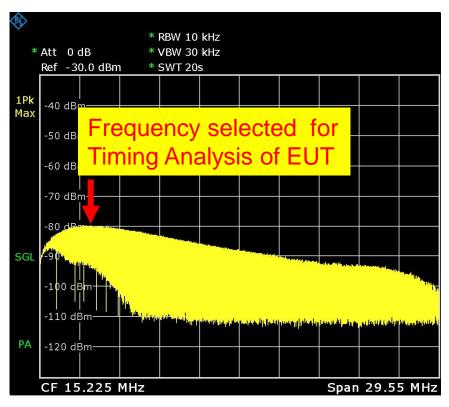
CISPR16-2 all parts – Measurement Time per Frequency



Even for a swept scan it is possible to discuss about a measurement time per frequency. This graph explains, how "CISPR A" understands the term measurement time at each frequency.



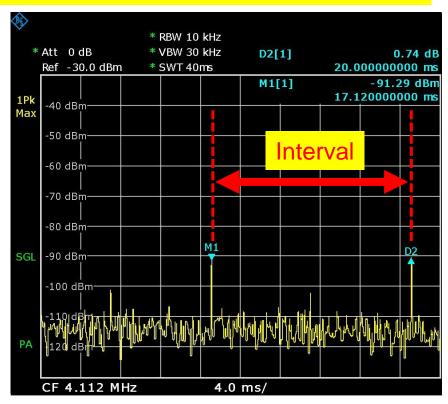
CISPR16-2 all parts – Interval between Pulses



Frequency sweep:

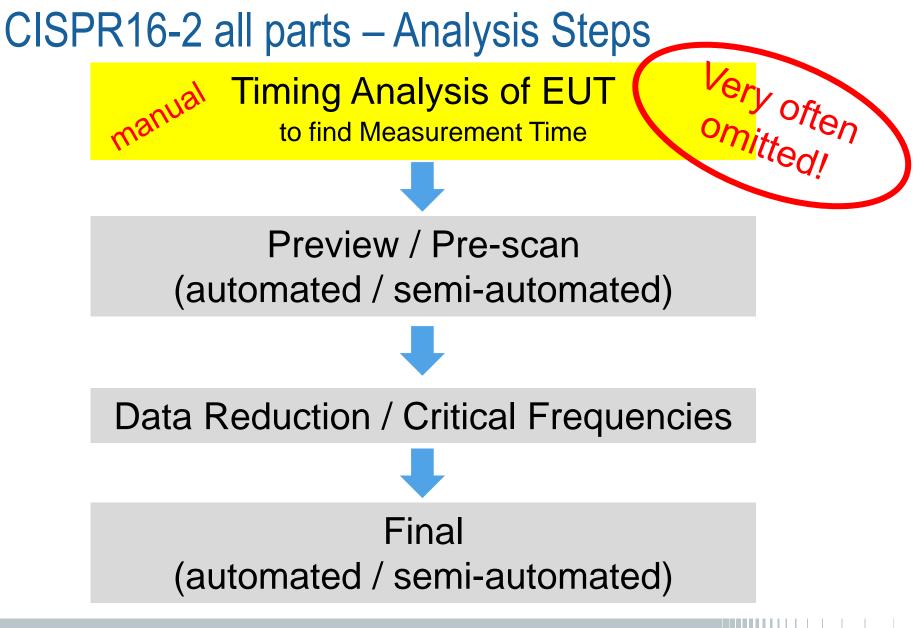
> 15 sec; around 6,000 points *) Thick trace \rightarrow intermittent signal

EUT: Interval between Pulses = 20 ms



ZERO SPAN mode: Analysis of EUT behavior in the time domain.

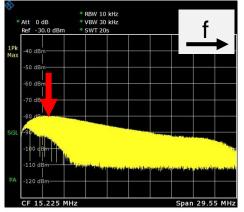
ROHDE&SCHWARZ





CISPR16-2 all parts – EUT Timing Analysis

Example Results



Date: 1.MAR.2013 19:33:38



Detector: Pos. Peak No. of points: e.g. approx. 6000 in Bd. B SWT = 15 s Thick trace: >> 2 dB

* BBW 10 kHz * Att 0 dB * VBW 30 kHz D2[1] 0.74 dB * Att 0 dB * SWT 40ns D2[1] 0.74 dB * Att 0 dB * SWT 40ns D2[1] 0.74 dB * Att 0 dB * SWT 40ns D2[1] 0.74 dB * Att 0 dB * SWT 40ns D2[1] 0.74 dB * Att 0 dB * SWT 40ns D2[1] 0.74 dB * 40 dB * SWT 40ns D2[1] 0.74 dB * 40 dB * SWT 40ns D2[1] 0.74 dB * 50 dB * SWT 40ns D2 D0 ms * 60 dB * 20 ms 0 0 * 90 dB * 0 dB 0 0 0 * 90 dB * 100 dB * 0 0 0 * 100 dB * 0 0 0 0 * 100 dB * 0 0 0 0 0 * 100 dB * 0 0 0 0 0 * 20 dB * 0 0 0 0 0 * 100 dB * 0 0 0 0 0

Date: 1.MAR.2013 19:25:54



Timing Analysis prior to the actual measurement For a stepped scan, the result of step 2 can be directly used.

Out of experience:

if the settings of CISPR 16-2-x are applied, a thick trace is a good indicator for an intermittent interferer.

Optional Step 3) for a swept scan Calculating the sweep time.

Measurement Parameter

Start Frequency	150 kHz
Stop Frequency	30 MHz
Bandwidth	
RBW	10 kHz
Stepsize*	
50% of RBW	5.0 kHz
Frequency Span	29.85 MHz
Calculated Number of Steps	
resp.	5970
Calculated Number of Frequency Points	
*)	
Measurement Time per Step <i>J</i>	20 ms
Total Observation Time	
=[MT per step] * [calc. Number of steps]	120 s



Discussion of Measurement Parameters

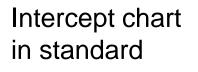
Measurement Parameter Spectrum Ana. 150 kHz to 30 MHz

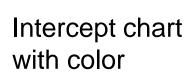
Start Frequency	150 kHz	
Stop Frequency	30 MHz	
Bandwidth		
RBW	10 kHz	
Stepsize*		
50% of RBW	5.0 kHz	
Frequency Span	29.85 MHz	
Calculated Number of Steps		
resp.	5970	
Calculated Number of Frequency Points		
Measurement Time per Step	20 ms	Result of step 2)
Table Observation Time		
Total Observation Time	100	Result of step 3)
=[MT per step] * [calc. Number of steps]	120 s	

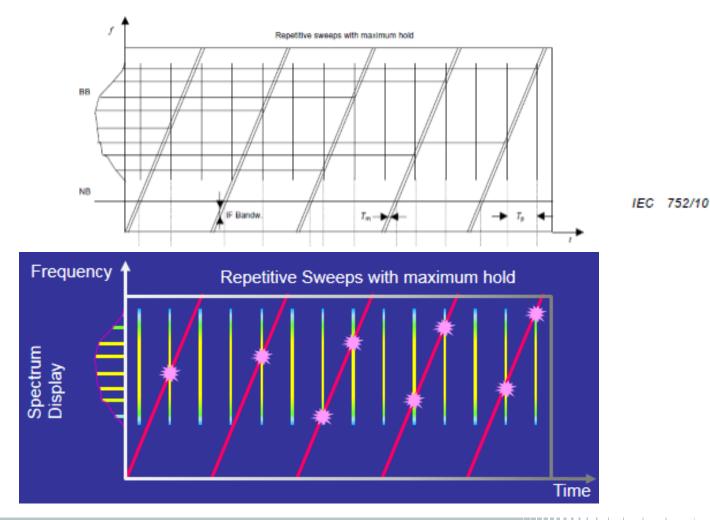
*) Even for a sweep it is strongly recommended to think in steps to determine the speed requirements.



CISPR16-2 all parts – since edition 1 Important Graph: Visualization of Interceptions



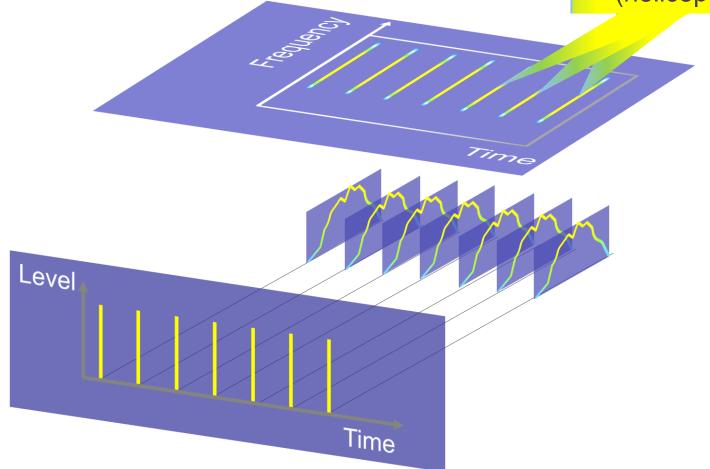




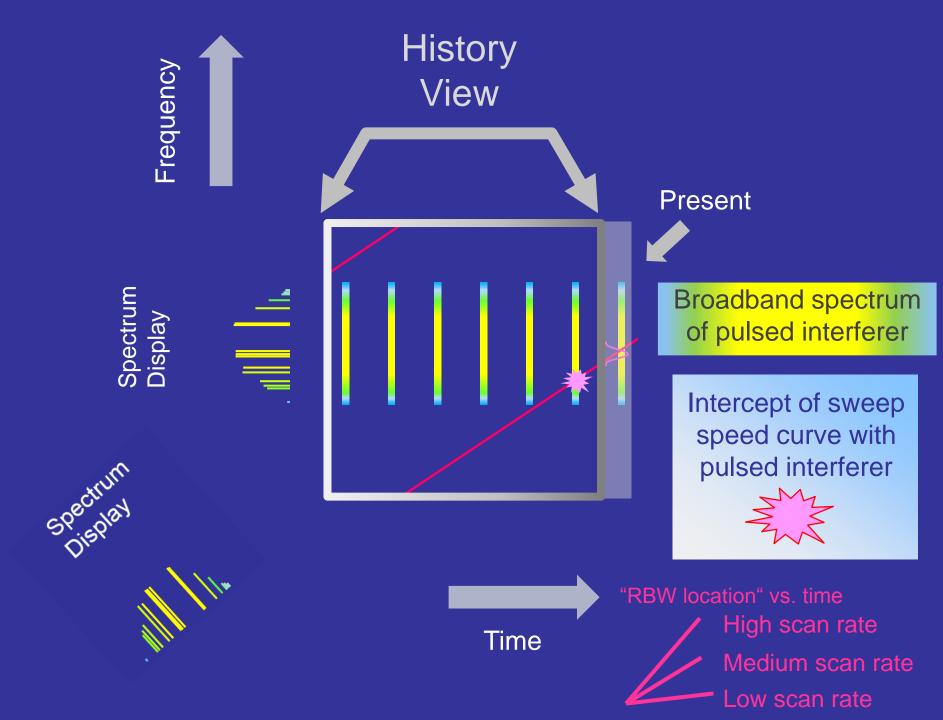


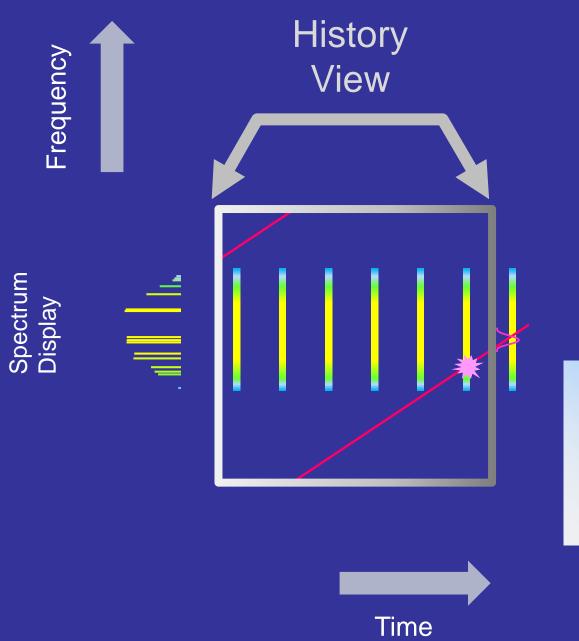
Intermittent Broadband Spectrum

Broadband spectrum of pulsed interferer (helicopter view)



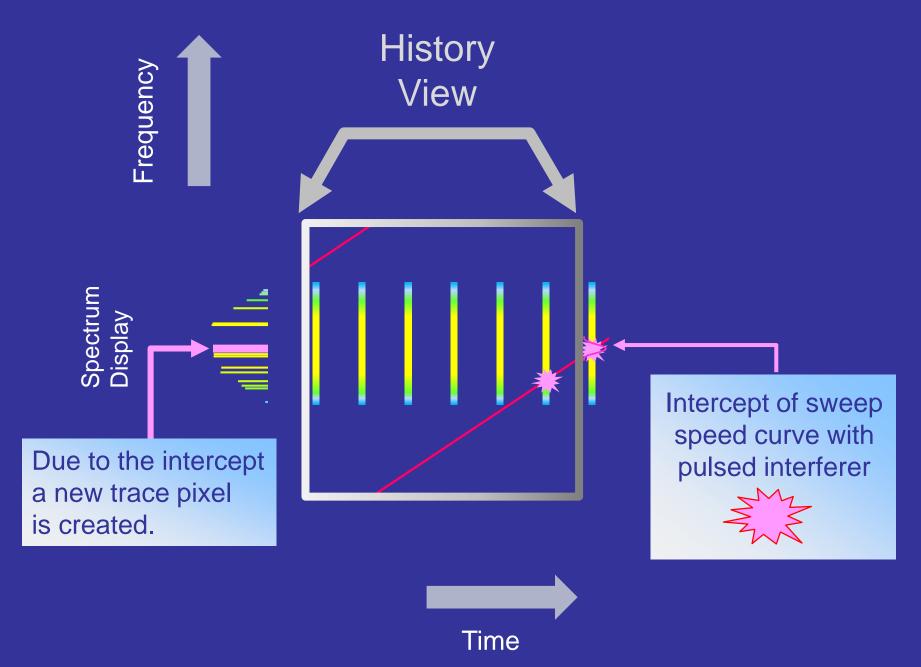


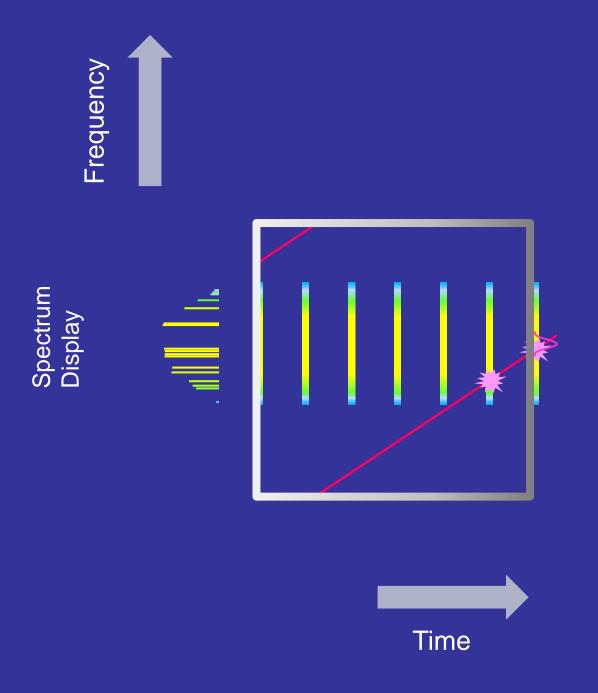


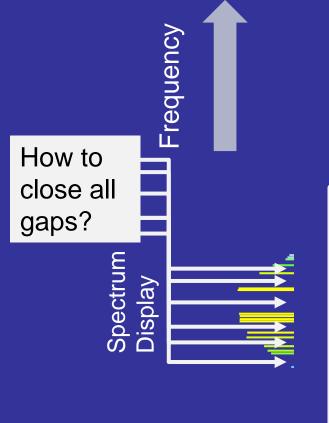


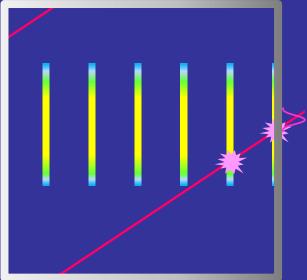
Intercept of sweep speed curve with pulsed interferer















EUT Timing Analysis to minimize Risk of Gaps

- The EUT Timing Analysis helps to find the correct measurement time per frequency
- For spectrum analyzers the measurement time per frequency translates into a sweep time setting
- For scanning receivers (stepped scan!) the measurement time per frequency translates into a dwell time.
- The correct settings will increase the match of the measurement curve with the "Spectrum Envelope"
- A gap smaller than 2 dB is regarded as a good match of the measurement curve with the Spectrum Envelope.



EUT Timing Analysis Step by Step

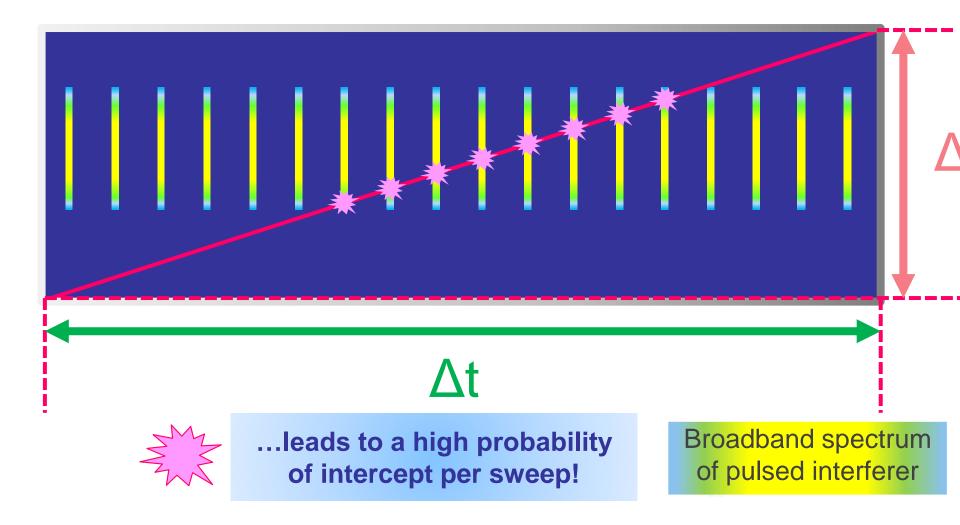
- Spectrum analyzer with sweep time = 15 sec
- Activate sufficient frequency points \rightarrow approach step size = 50% of RBW
 - CISPR Band B: 6000 @ RBW = 9 kHz
 - CISPR Band C/D 16000 @ RBW = 120 kHz
 - If the analyzer can not handle such amount of points then the span has to be reduced accordingly
- Trace Detector: Max Peak or Positive Peak
- Single Sweep
- Check for a "thick trace" e.g. > 10 dB. This is an indicator for an intermittent signal (pulsed signal)
- Place a marker on a high level of the thick band in the display
- Select the marker frequency as the new center frequency
- Switch to "zero span".
- Modify the sweep settings: e.g. sweep time (time window span) = 100 ms
- Find out the interval between two pulses / trenches, etc.
- In case of irregular peak patterns select a sweep time, where often 5 peaks occur in the display. Then divide the sweep time by 4 to get a useful measurement time per frequency point.

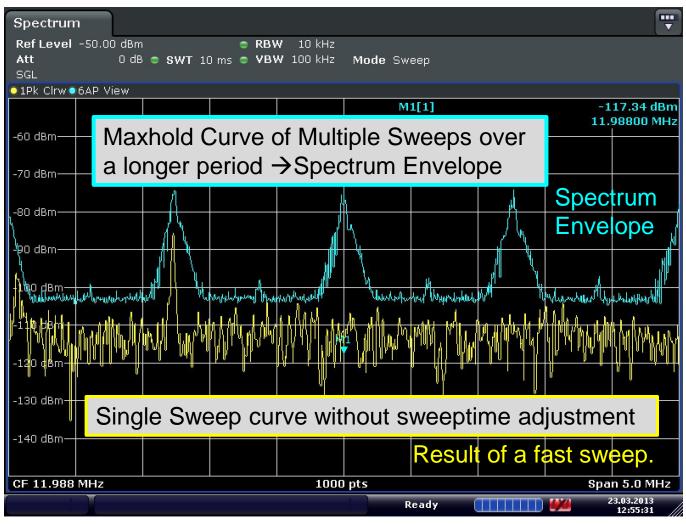


Signal Interception

$\Delta f / \Delta t$

A low scan rate...



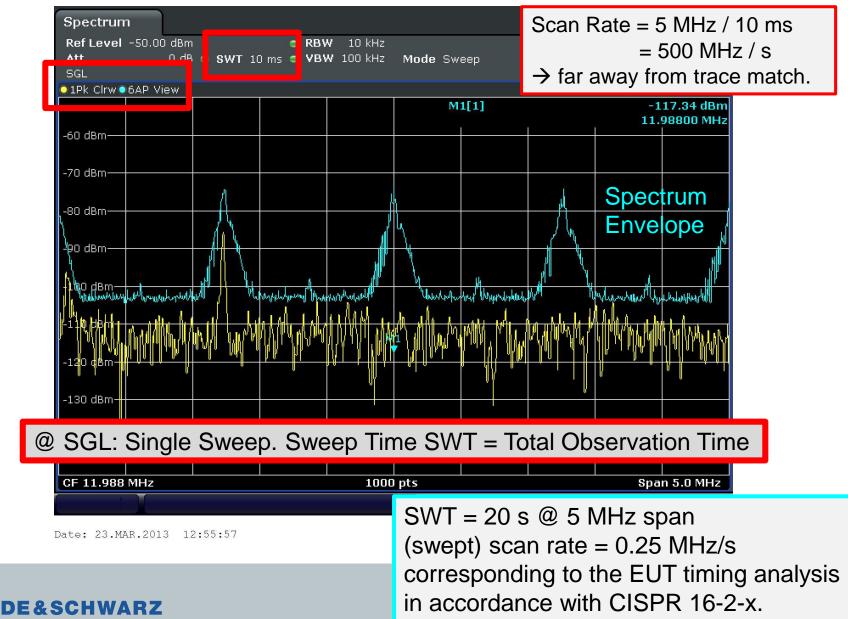


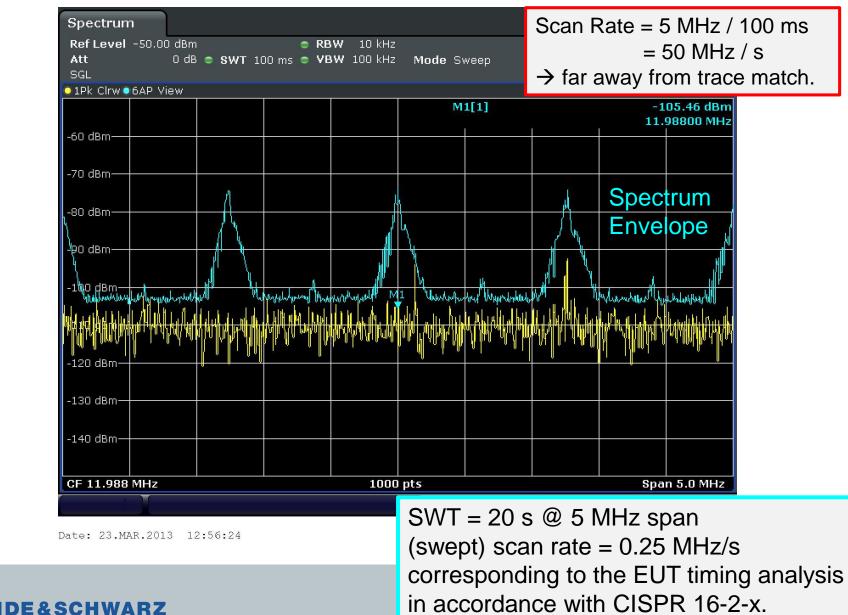
Date: 23.MAR.2013 12:55:31

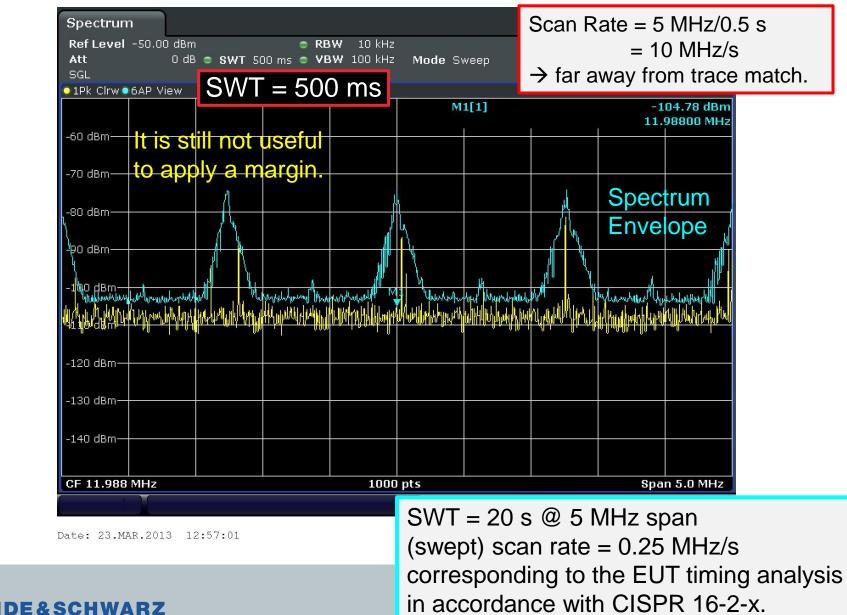


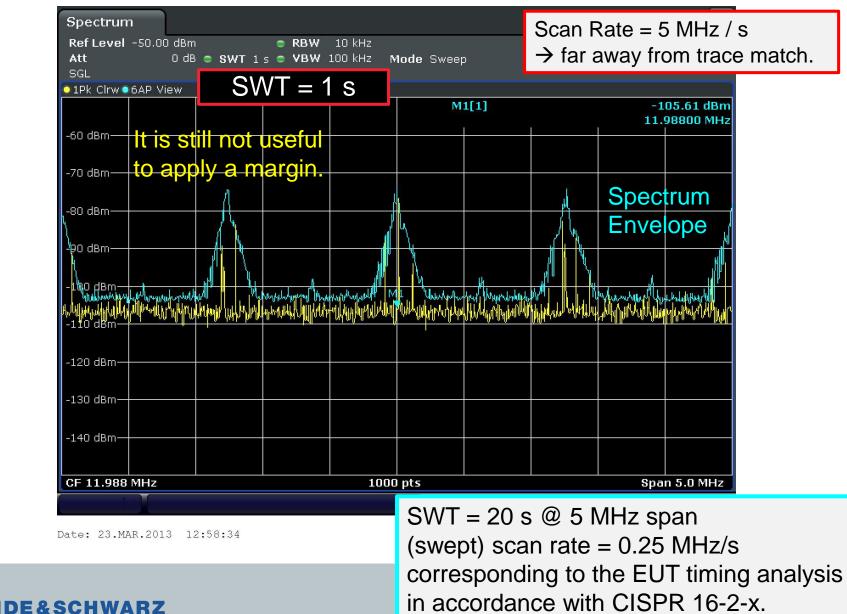
Start Frequency A focus on a smaller 9.488 MHz Stop Frequency frequency range has 14.488 MHz Bandwidth been decided by the 10 kHz RBW user to achieve a better 10 kHz Stepsize* 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 20 s	Measurement Parameter Spectrur			rum An	a. 5 MHz S	Span in Bd. B
Stop Frequency frequency range has been decided by the user to achieve a better visualization. 10 kHz Stepsize* 10 kHz 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps resp. 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 5.00 ms	Start Frequency			9	.488 MHz	
Bandwidth been decided by the user to achieve a better visualization. Stepsize* 10 kHz 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps resp. 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 1000	Stop Frequency			14	1.488 MHz	
RBW user to achieve a better 10 kHz Stepsize* 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 10						J
Stepsize* 5.0 kHz 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 1000		been decided by t	the			
Stepsize* 50% of RBW 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 1000	RBW	user to achieve a better			10 kHz	
Stepsize* 50% of RBW 50% of RBW 5.0 kHz Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 1000 Measurement Time per Step 20 ms Total Observation Time 1000		visualization.				
Frequency Span 5.00 MHz Calculated Number of Steps 1000 Calculated Number of Frequency Points 20 ms Measurement Time per Step 20 ms Total Observation Time 1000				┛		
Calculated Number of Steps 1000 resp. 1000 Calculated Number of Frequency Points 20 ms Measurement Time per Step 20 ms Total Observation Time 1000	50% of RBW				5.0 kHz	
Calculated Number of Steps 1000 resp. 1000 Calculated Number of Frequency Points 20 ms Measurement Time per Step 20 ms Total Observation Time 1000	Frequency Span				5.00 MHz	
resp. 1000 Calculated Number of Frequency Points 20 ms Measurement Time per Step 20 ms Total Observation Time 1000		er of Stens			0.00 1/11/2	
Calculated Number of Frequency Points Measurement Time per Step 20 ms Total Observation Time	·				1000	
Total Observation Time						
Total Observation Time	Measurement Time per Step				20 ms	
					201115	
=[MT per step] * [calc. Number of steps] 20 s	Total Observation Time					
	=[MT per step] * [calc. Number of steps]				20 s	

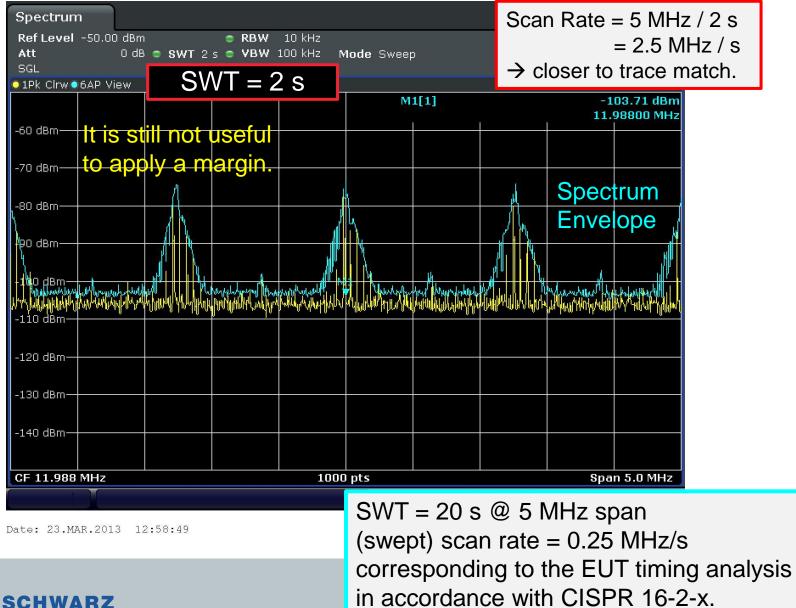




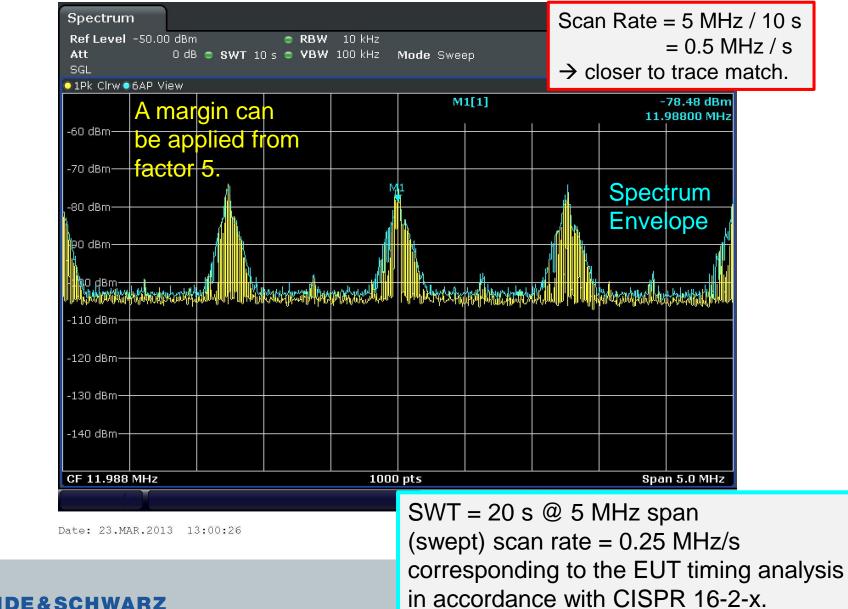


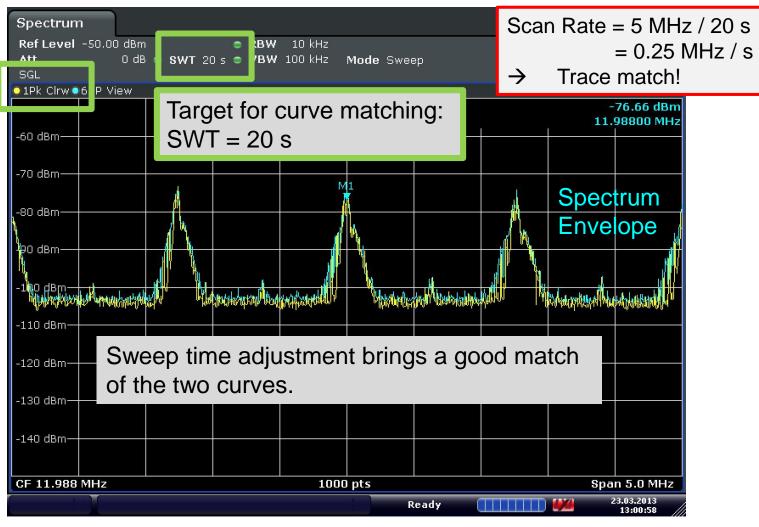












Date: 23.MAR.2013 13:00:58



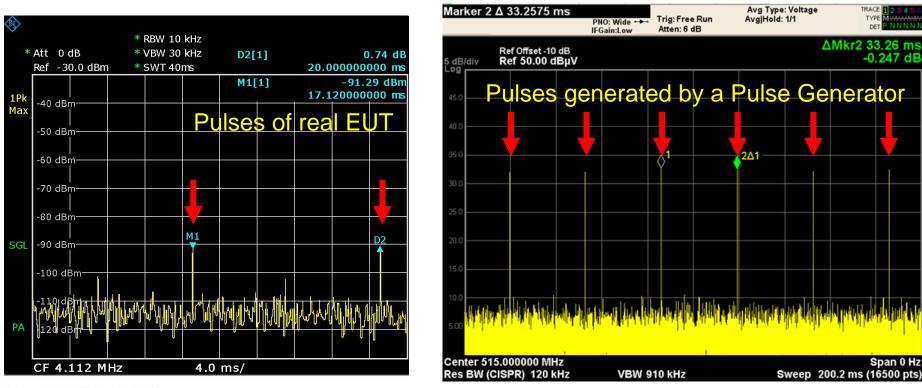
EUT Timing Analysis to increase Repeatability

- The EUT Timing Analysis helps to find the correct measurement time per frequency
- Fast sweeps without understanding the pulse interferer characteristic of the EUT just result in "lucky shots".
- The measurement reliability is shrinking with fast sweeps / scans applied to unknown EUT. Critical frequency points can be missed.
- Subranges might be represented not at all or with values that are far below the actual interferer subrange maximum



Pulse Generators

help to prove CISPR 16-2-x Strategy to find the correct Observation Time



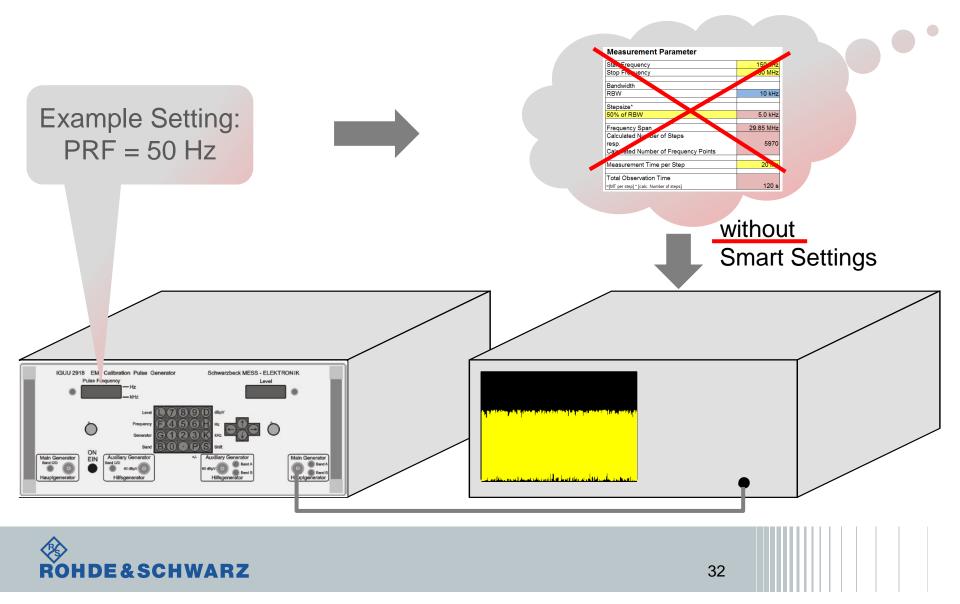
Date: 1.MAR.2013 19:25:54

Instrument settings: spectrum analyzer in ZERO SPAN mode The signals are analyzed in the time domain.



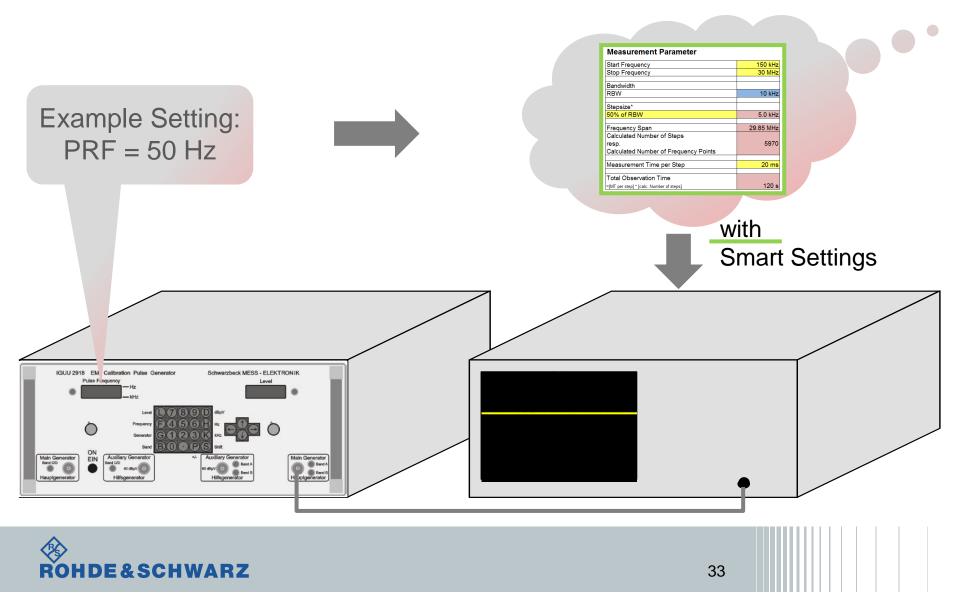
Pulse Generators

help to prove CISPR 16-2-x Strategy to find the correct Observation Time



Pulse Generators

help to prove CISPR 16-2-x Strategy to find the correct Observation Time



Measurement Parameter **Pulse Generators** 150 kHz Start Frequency Stop Frequency 30 MHz By means of classic technology long observation times have to Bandwidth be accepted to avoid gaps in the RBW 10 kHz spectrum envelope. Stepsize* 50% of RBW 5.0 kHz Example Setting: 29.85 MHz Frequency Span PRF = 50 HzCalculated Number of Steps 5970 resp. MT = 1/PRFCalculated Number of Frequency Points Measurement Time per Step 20 ms **Total Observation Time** 120 s =[MT per step] * [calc. Number of steps] GUU 2918 EM Calibration Pulse chwarzbeck MESS - ELEKTRONI Main Generator Bant A Bant B Huptgenerator

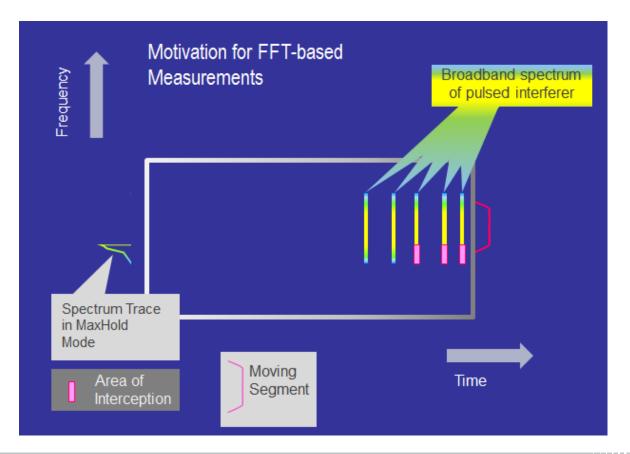
34

DE&SCHWARZ

Motivation for FFT-based Measurements

Request for shorter oberservation times

The interceptions will change from interception points to interception areas





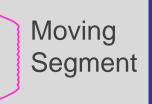


Motivation for FFT-based Measurements

Broadband spectrum of pulsed interferer



Area of Interception





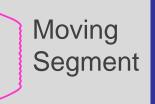


Motivation for FFT-based Measurements

Broadband spectrum of pulsed interferer

Spectrum Trace in MaxHold Mode

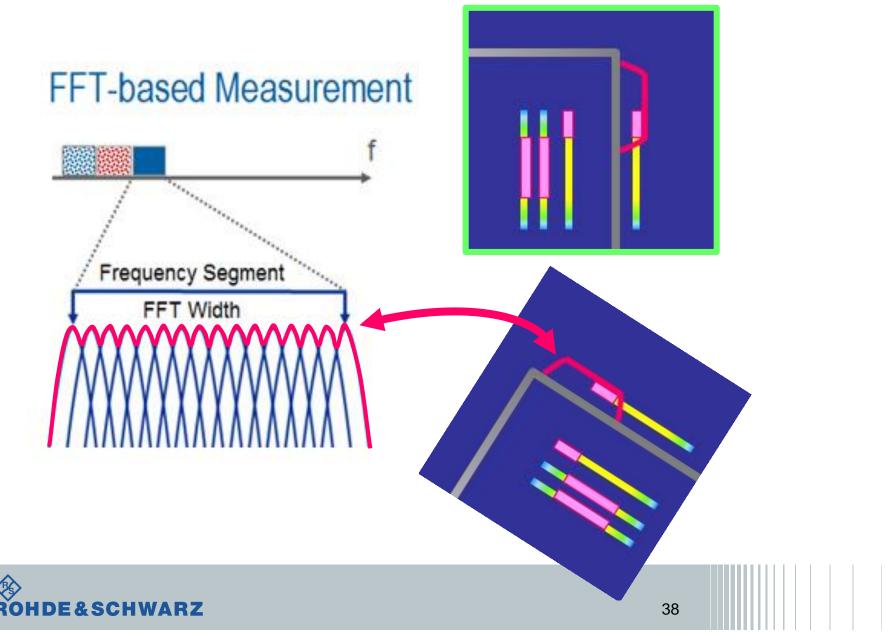
> Area of Interception



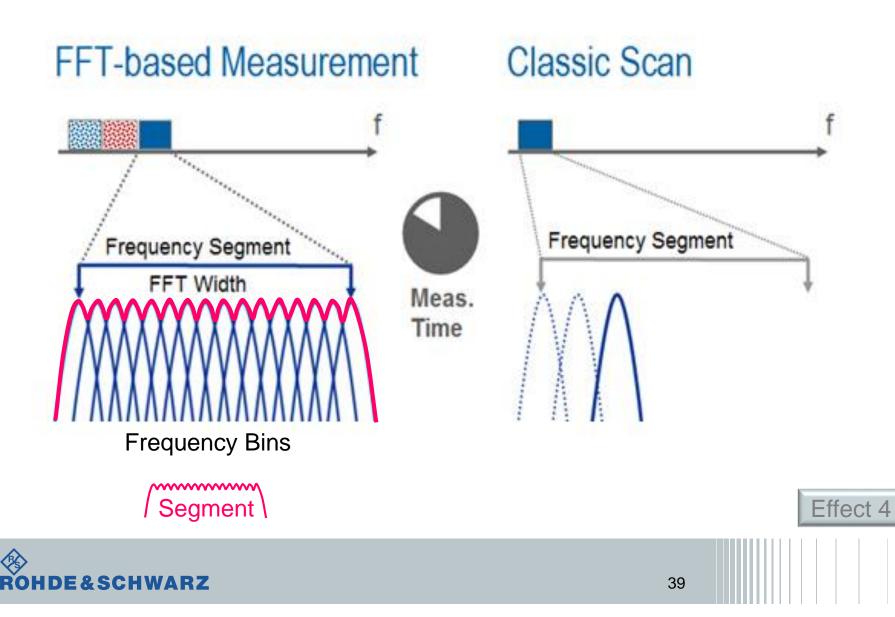




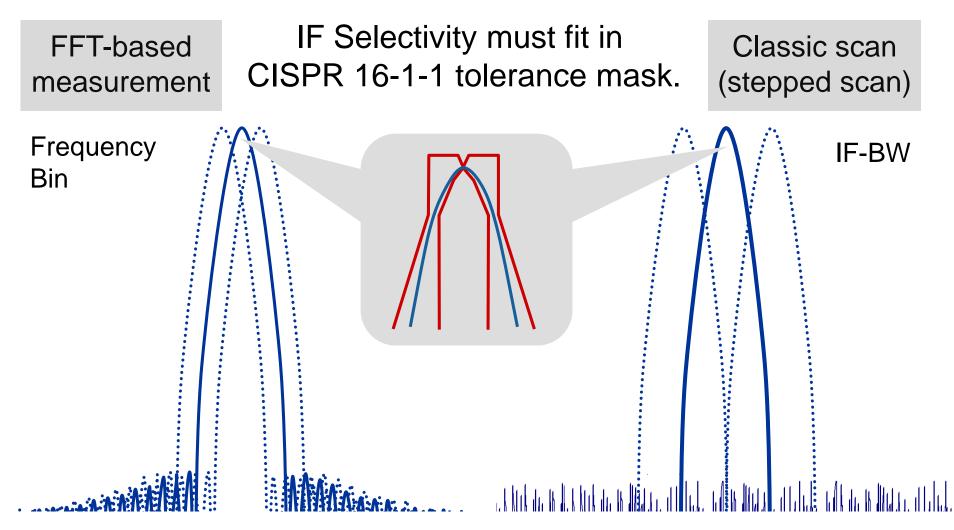
Motivation for FFT-based Measurements

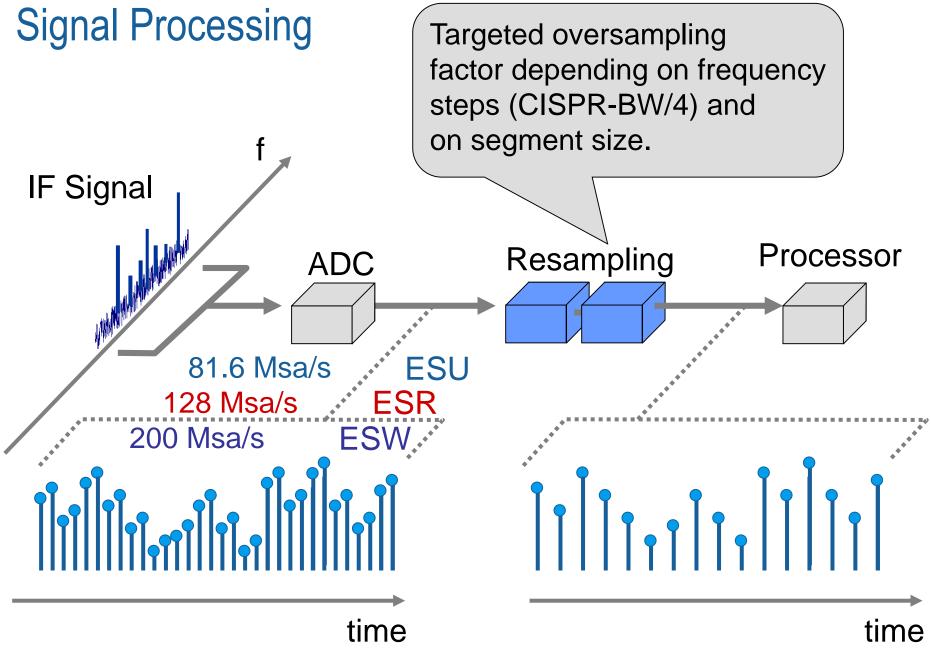


Motivation for FFT-based Measurements

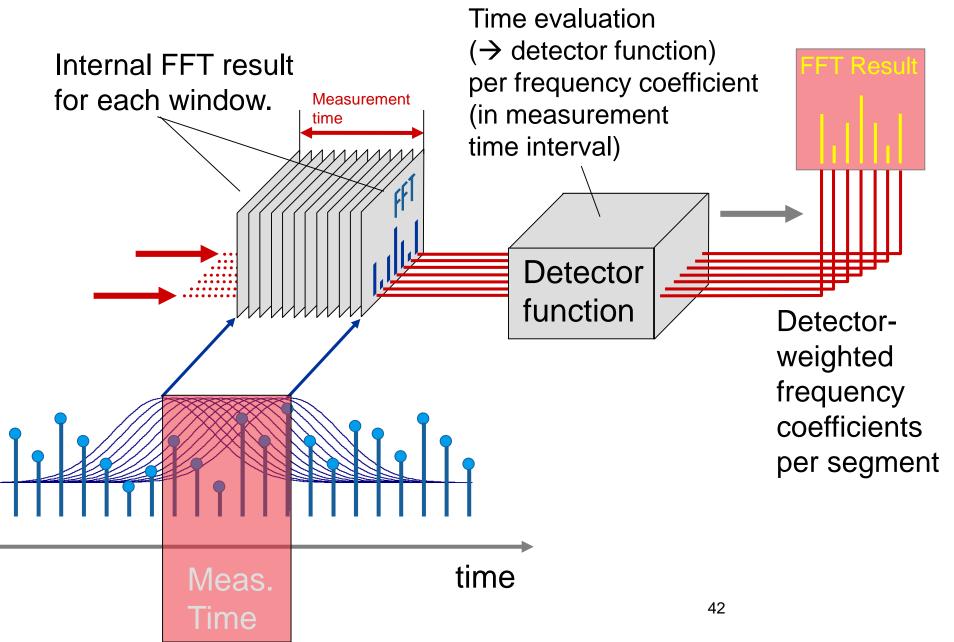


Accuracy Requirement for Frequency Bins

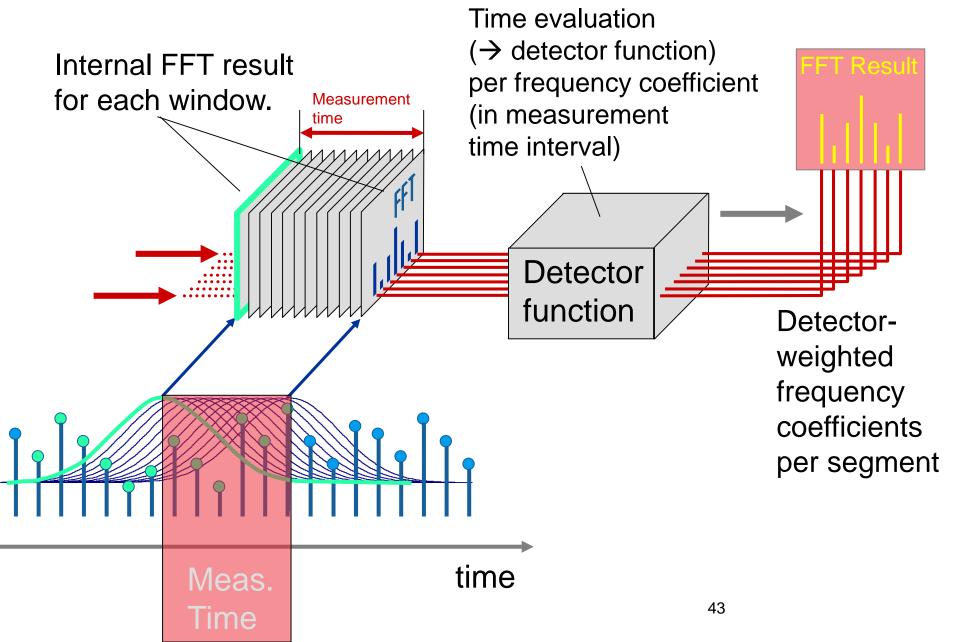




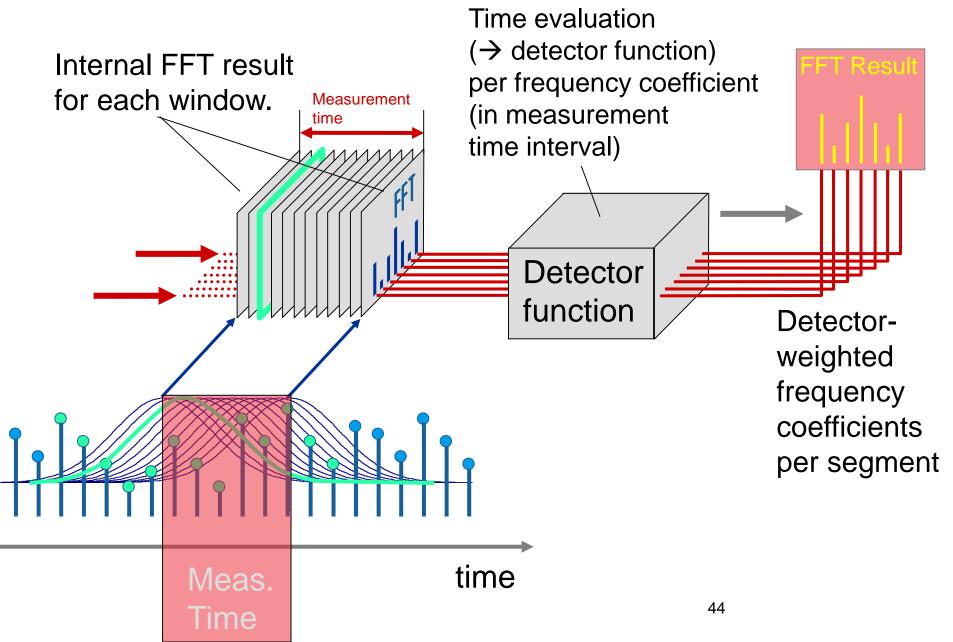
Signal Processing

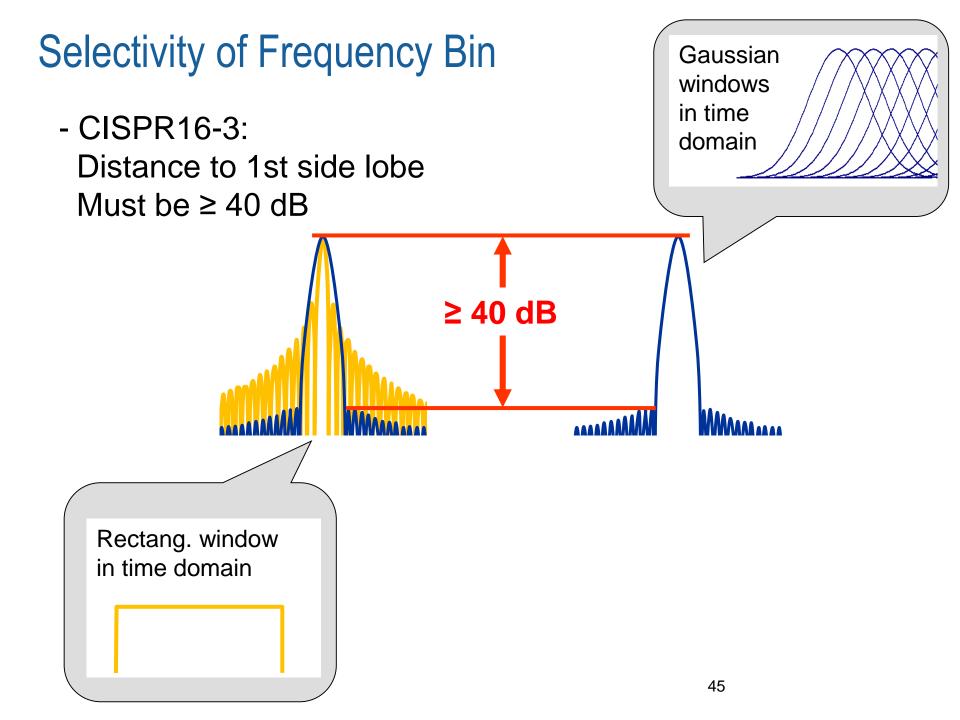


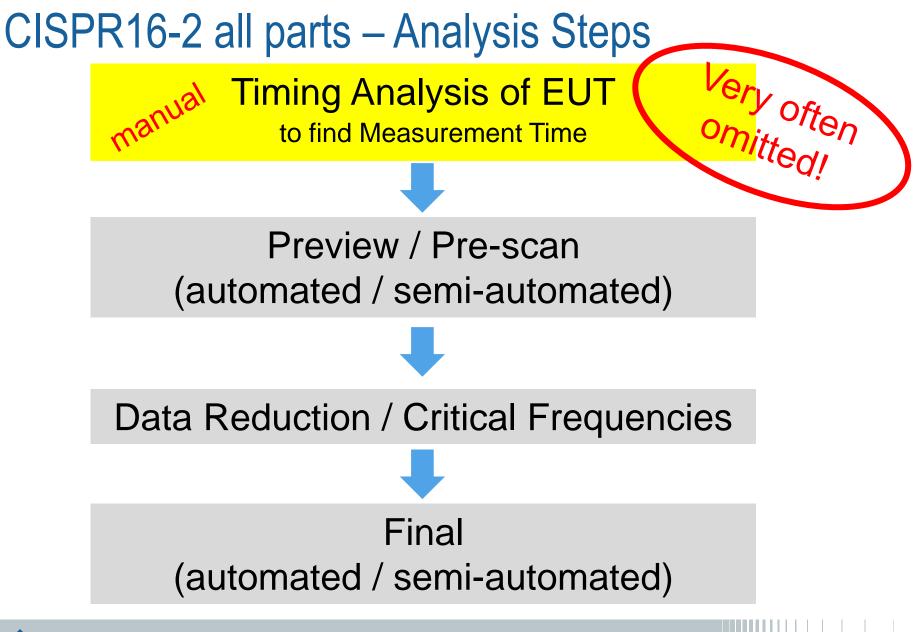
Signal Processing



Signal Processing











TV Set near power connector; transducer nearfield probe





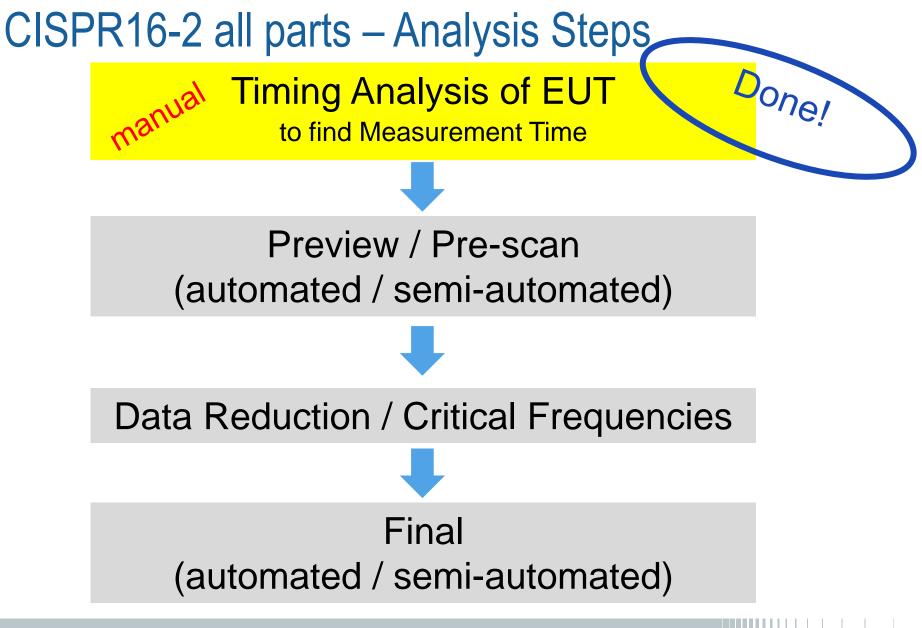
TV Set near power connector; transducer nearfield probe



Receiver		-Time Spectrum	8	
Input 1 AC	Att 0 dB Preamp 0	dB Step TD Scan		
Level	dBµV	Fr	equency	/ 500.0000000 MHz
Max Pe	ak 5.42 -10	10	30	50 70 90
Scan 🔵 1P	k Clrw			4
45 dBµV		100 MHz	D2[1] 	7.98 dB 23.400000 MHz 9.36 dBµ¥ 30.060000 MHz
40 dBµV	Measurement Tim The EUT Time Be result has been dis	havior Che	ck —	Analysis of the EUT time behavior at the Center Frequency 133.269 MHz in ZERO SPAN mode.
20 dBµV	WWWW	A . Allan		binding downed different of the providence of this on the providence of the providen
ло феру 5 dBµV 0 dBµV	manipunant	M Marine	hummethingthin	Stimulus Response Function Function F 92,5461 ms 13.35 dBy/ Function F Function F 9,99 ms -1.79 dB Function F Function F 19,9911 ms 2.16 dB Function F Function F 29,9922 ms -3.11 dB Function F Function F
-5 dBµV	MHz			TF Stop 500.0 MHz
			Measuring	11.04.2013 21.39:26

TV Set near power connector; transducer nearfield probe







Ref Level 77.00 dBj	ectrum X µV • dB • SWT 100 ms	RBW 100 kHz VBW 100 kHz	Input 1	AC	
a measure of at least	n out of ZER ment time or 10 ms per fre ment time of	r observat equency p	tion time point is r	equired.	-3.11 dB 29.9922 ms 13.35 dBµV 32.5481 ms
20 dBµV			D4		
			han a shi ka a sa		
CF 133.269 MHz		9000 pts	5		10.0 ms/
Marker					
Type Ref Trc	Stimulus	Response	Function	Function F	Result
M1 1	32.5481 ms	13.35 dBµV			
D2 M1 1	9.99 ms	-1.79 dB			
D3 M1 1 D4 M1 1	19.9911 ms	2.16 dB -3.11 dB			
D4 M1 1 D5 M1 1	29.9922 ms 39.9822 ms	2.08 dB			
			Deadu		11.04.2013
			Ready		21:04:27
TV Set near	r power conr	nector; tra	Insducer	nearfield pr	obe



Sufficient Measurement Time → Intercept OK



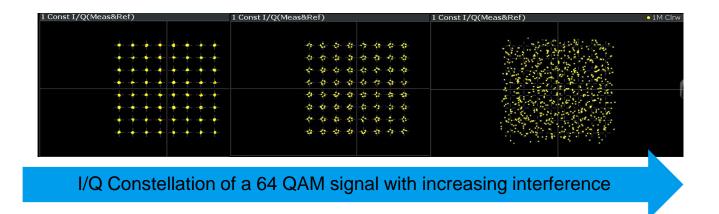
TV Set near power connector; transducer H-nearfield probe



Why RSE become really important measurements

Motivation: getting less EM pollution in the air

- Spurious (interferers) decrease systems performance
- This is the only way to get efficient cohexistence between systems which use same frequencies list shared in time





EMI and RSE differences regarding measurements

ERP: Effective radiated power

The measured quantity to be evaluated is not the electric field radiated but the effective radiated power not at the location of the measurement antenna but from the EUT.

Therefore, the

level in **dBµV** measured on the receiver instrument must be converted to **dBm** differently than in standard EMI measurements (dBµV/m) and the free space attenuation for a given measurement distance (d) has to be considered.

Consequences : different transducer factors tables

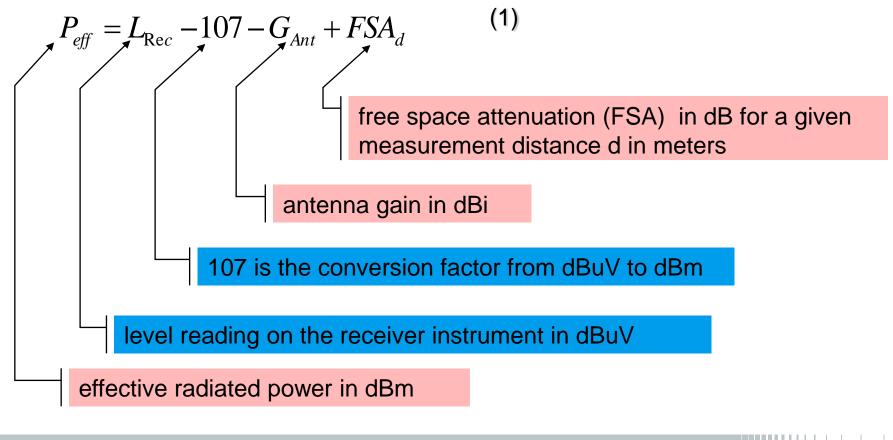
have to be derived for the antenna transducer factor (TF) in antenna properties, which describes the antenna's signal conversion characteristic.



EMI and RSE differences regarding measurements

Range Attenuation (theoretical)

The power effectively radiated from a mobile phone at a certain frequency is given by:





Field and Space

Wrong polarisation can make infinite attenuation

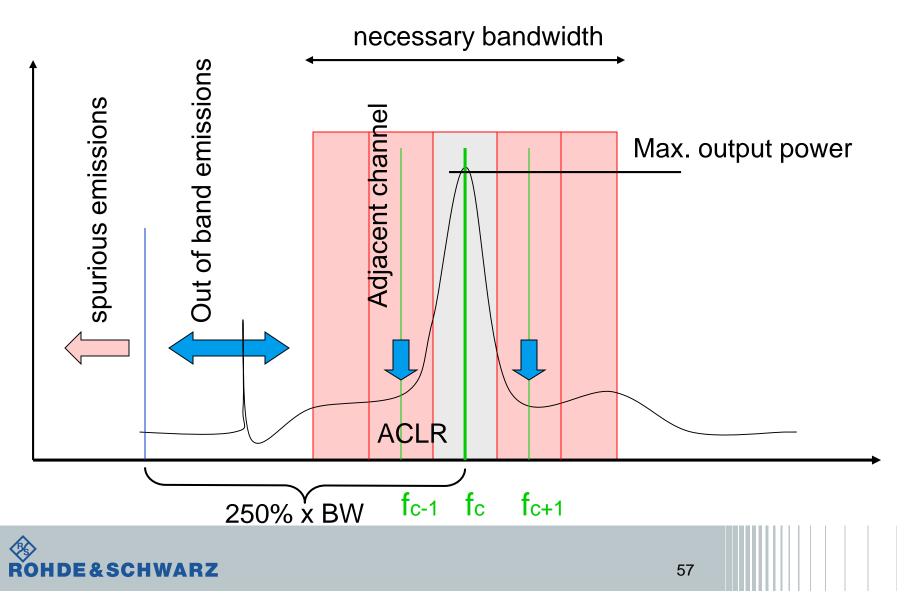


	Î		$\langle \rangle$	G
V ↑	0 dB	8	3 dB	3 dB
Τ	8	0 dB	3 dB	3 dB
RHC	3 dB	3 dB	0 dB	8
LHC	3 dB	3 dB	8	0 dB



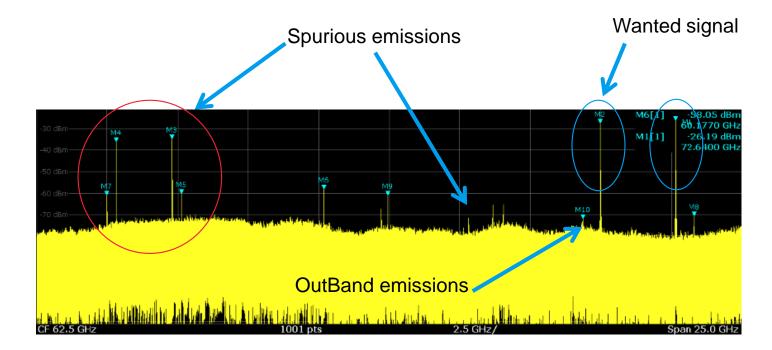
Spurious Emissions <> Emissions Mask functions

CP/ACP >> OutBand >> Spurious



Spurious Emissions <=>Emissions Mask functions

- Unwanted emissions outside the transmitter nominal operation frequency. Exclude the out of band emissions
- Caused by harmonic emissions, parasitic emissions, intermodulation products and frequency conversion products.

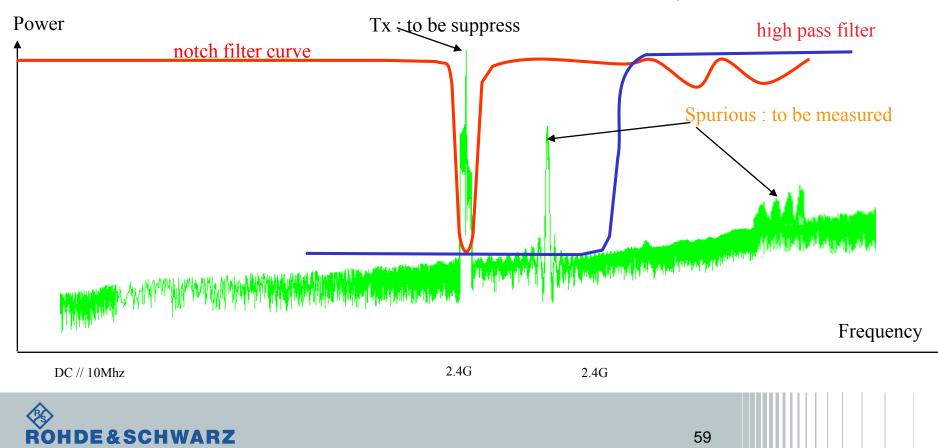




Spurious Emissions and RF power consideration

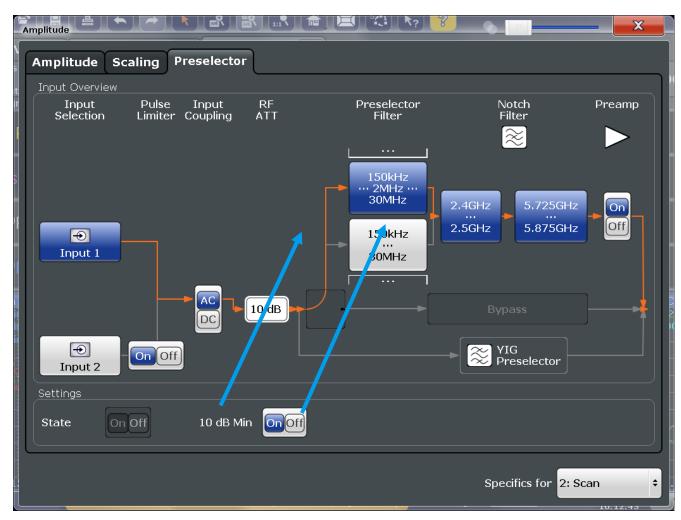
TX power = risk of Overload instrument

- I Notch filter to reject the Transmetter Carrier (but BW limited most of time)
- I HighPass filter, which can have passband up to 26 or 40 Ghz...
- Last, you can use antenna response to make this filtering



Spurious Emissions on EMI receiver(latest ESW)

- I Internal Notch filter (2.4Ghz & 5Ghz) added to classic CISPR Preselector
- I Internal PA

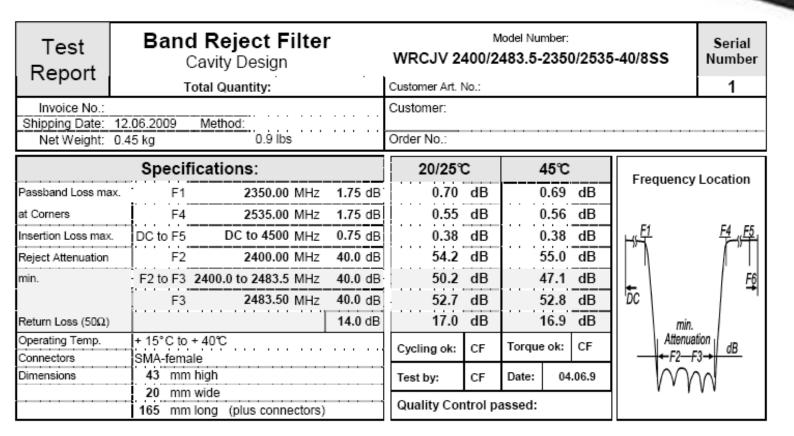




Spurious Emissions on Spectrum Analyser

- External Notch filter, if not enough dynamics
- I Internal PA if not enough DANL on the SA

(both need dedicated calibration)





Spurious Emissions and Time consideration

Good Noise floor = narrow RBW (if not standardized) Meas. speed = but linked to the Rbw/Span

	Range 1	Range 2	Range 3	Range 4
Range Start	30 MHz	5.75 GHz	6.25 GHz	13 GHz
Range Stop	5.75 GHz	6.25 GHz	13 GHz	26 GHz
Spur Detection Threshold Start	-120 dBm	-30 dBm	-120 dBm	-100 dBm
Spur Detection Threshold Stop	-120 dBm	-30 dBm	-120 dBm	-100 dBm
Limit Offset to Detection Threshold	0 dB	0 dB	0 dB	0 dB
Peak Excursion	3 dB	3 dB	3 dB	3 dB
Minimum Spur SNR	10 dB	10 dB	10 dB	10 dB
Maximum Final RBW	100 kHz	100 kHz	100 kHz	100 kHz
Auto RBW	On	On	On	On
RBW	Auto	Auto	Auto	Auto
Number of FFT Averages	2	2	2	2
Ref Level	0 dBm	0 dBm	0 dBm	0 dBm
RF Attenuation	10 dB	10 dB	10 dB	10 dB
Preamp	Off	Off	Off	Off

Spectrum mode : Sweep list

Receiver mode : Scan table

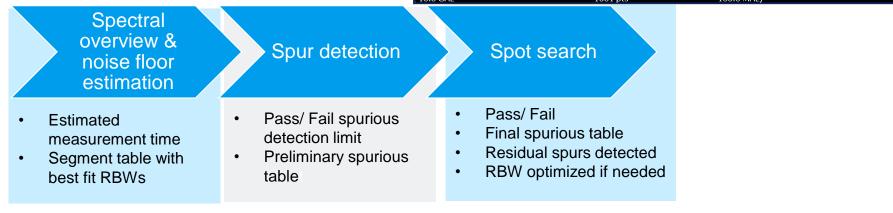
Overview 5	Scan Table	Peak \$	Search	Trac	e/Final	Meas	LISN Settin	ngs
Scan Start	150.0 kHz		Time	Dom	ain Scan	OF	E ON	
Scan Stop	7.0 GHz		Ad	just A	xis	Del	lete Range	
Step Mode	AUTO	\$	Insert F	Range	Before	Insert	t Range Aft	er
	Range 1		R	ange	2		Range 3	
Range Start	(150.0 kHz		30.0 Mł	Ηz)	1.0 G	Hz	
Range Stop	30.0 MHz		1.0 GHz	!		7.0 G	Hz	
Step Size	2.25 kHz		30.0 kH	lz		250.0	kHz	
Res BW	9.0 kHz		(120.0 k	Hz		1.0 M	Hz	
Meas Time	(1 s		(100 ms	})	(10 ms	5	
Auto Ranging	OFF O	N	OFF		ON	OF	F) ON	
RF Attenuation	(10 dB		0 dB			0 dB		
Preamplifier	AUTO	¢	AUTO		\$	AUTO		\$
RF Input			1		2		2	



Spurious Emissions (RBW versus sweep time)

- The smaller the resolution bandwidth, the higher the spectral resolution.
- The RBW influences the displayed noise floor and the sweep speed of the spectrum analyzer.

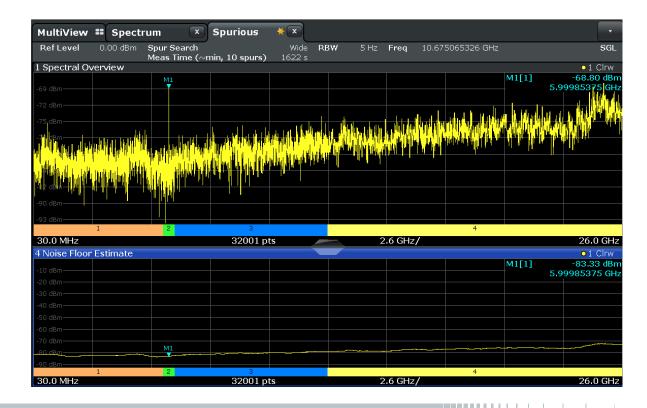
Ref Level -60.00 dBm		RBW 3 MHz							
	SWT 4 ms	VBW 3 MHz	Mode Auto						
l Frequency Sweep				O 1PK A	vg • 2Pk Vie	w o3Pk View	• 4Pk View	● 5Pk View	● 6PK V
		and Mr. and marked a	Names and an and a start				there a device have a se		
municipalities	W-Ward-reduce			and the shares of the	manaherra	S. Walder and a contra	and a first of the second	and a second second second	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
-90 dBm									
	www.www.	djanderender och	mangenter		have been and the second	www.www.www.	mound	munimentaria	
		mundanta	angeles angely same on	Norman and Ambrances a			an water and		
hollowangenergenergenergenergenergenergenergen	MARY MARY MA				deressed subsecting	de la complete de la			-protection
Martin Marine Martin Contraction	and marsham	angen an	and a start a start and a start a start and a start a start as	the mark we	a that recommence	han be welling	. J. Mar May day May Sugar	was marine and	a bara da
	And the second sec							A A HULL MARK	nandra og i Ali viði
-120 dBm	an a transmis	. Loss Nac Aubara	A walking another of				واللا استاسية المرا	and a set	
-l-montespectifications	A Carrier and a contraction	Contraction des contracts of		. a. A. market of a start of a	-navanara - waa	w ^a llan on the same and the second	da oorde te de la deste la deste de la deste de la	AL A PROVING PORT	mondar
-130 dBm									
			an many marghan da						
10.0 GHz		10	001 pts		100.0 M	Hz/			11.0





Spurious Emissions (prescan as overview)

- Measures noise floor for user settings
- Estimates required measurement time
- Calculates optimum RBWs for each frequency according to the spurious detection threshold





Spurious Emissions (spurious detection to limit line)

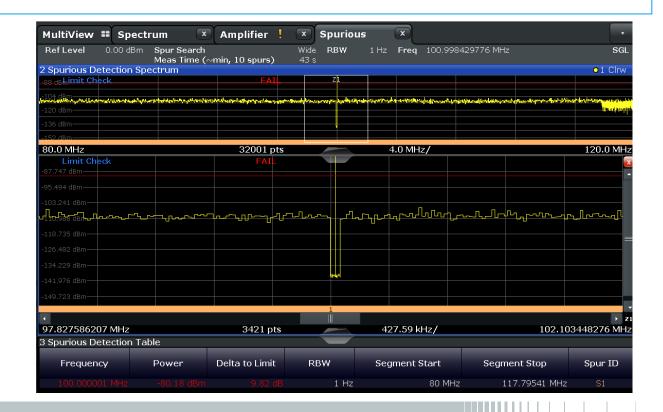
- Uses RBW settings calculated in previous sweep
- Preliminary spur table is the result

		<u> </u>					
Ref Level 0.0		Search	min, 10 spurs)	Wide RBW 1622 s	1 Hz Freq 333.51294	8412 MHz	S
Spurious Detec			min, to spurs)	1022 \$			o1 Clr
Limit Check	aon opeed ar	"	PASS				
) dBm							
				Remeasuring potential			
				ig RBW to achieve Spur			
) dBm							
		- 1 m					
	i	ail j					
)0,dBm	1						
				and the state of the	والمادية واللهم والمعرجة والمحمد والألحد والمحمد	بالجزر بيجافي والقوم والقروم والجرر والمرد بالمصال المحق التجاف	بالتوقيق والارجام
10 dBm					فالثلاث انتثب عنته كالالتنائب اللبي استعادهم تنتع		
- II - I							
in dem	يوريا فأطنانه ومريد			and the second			
10 dBm	an a	and the second second					
	a	and the second s					
40 dBm	ann an						
+0 dBm		2	3			4	
10 dBm		2	3 32001 pts		2.6 GHz/	4	26.0 0
10 dBm		2	Ŭ		2.6 GHz/	4	26.0 0
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	RBW			_
+0 dBm			Ŭ	RBW	2.6 GHz/ Segment Start	4 Segment Stop	26.0 G Spur ID
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz	Segment Start 30 MHz	Segment Stop 1.378772513 GHz	Spur ID S1
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz	Segment Start 30 MHz 30 MHz	Segment Stop 1.378772513 GHz 1.378772513 GHz	Spur ID S1 S2
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz 8 Hz 8 Hz 8 Hz	Segment Start 30 MHz 30 MHz 30 MHz	Segment Stop 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz	Spur ID S1 S2 S3
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz 8 Hz 8 Hz 8 Hz	Segment Start 30 MHz 30 MHz 30 MHz 30 MHz 30 MHz	Segment Stop 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz	Spur ID \$1 \$2 \$3 \$4
D dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz 8 Hz 8 Hz 8 Hz 8 Hz 8.9 Hz	Segment Start 30 MHz 30 MHz 30 MHz 30 MHz 1.378772513 GHz	Segment Stop 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 4.203111665 GHz	Spur ID S1 S2 S3 S4 S5
10 dBm 1 D.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz 8 Hz 8 Hz 8 Hz 8.9 Hz 10.9 Hz	Segment Start 30 MHz 30 MHz 30 MHz 30 MHz 1.378772513 GHz 4.970216126 GHz	Segment Stop 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 4.203111665 GHz 5.75 GHz	Spur ID \$1 \$2 \$3 \$4 \$5 \$6
0.0 MHz Spurious Detec	tion Table		32001 pts	8 Hz 8 Hz 8 Hz 8 Hz 8 Hz 8 Hz 8.9 Hz	Segment Start 30 MHz 30 MHz 30 MHz 30 MHz 1.378772513 GHz	Segment Stop 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 1.378772513 GHz 4.203111665 GHz	Spur ID S1 S2 S3 S4 S5



Spurious Emissions (partial sweep as spot search)

- Performed over very narrow spans around each spur detected in the previous step
- Pass/ Fail considering spurious emissions limit and SNR
- Final spurious table





Spurious Emissions (test time divided by 44)

Spur search with the new FSW-K50 is up to 50 times faster than traditional spurious

RBW / Noise (dBm) 1 GHz span	High end spectrum analyzer Speed (s)	R&S FSW spectrum analyzer, Speed (s)	New FSW-K50 Spurious search application Speed (s)
1 Hz / -140	9700	12246	200
2 Hz / -138	2840	3088	84
3 Hz / -135	1470	1384	35
5 Hz / -132	660	507	12
10 Hz / -130	308	132	7
20 Hz / -128	126	36	6
30 Hz / -125	51	17	5
50 Hz / -122	42	7.1	4
100 Hz/-120	23	4.1	3



